UNCLASSIFIED

AD NUMBER AD038959 LIMITATION CHANGES TO: Approved for public release; distribution is unlimited. FROM: Distribution authorized to U.S. Gov't. agencies and their contractors; Administrative/Operational Use; AUG 1954. Other requests shall be referred to Office of Naval Research, Washington, DC. AUTHORITY ntis onr ltr, 26 oct 1977

UNCLASSIFIED

AD 38959

DEFENSE DOCUMENTATION CENTER

FOR

SCIENTIFIC AND TECHNICAL INFORMATION

CAMERON STATION ALEXANDRIA. VIRGINIA



UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U.S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the helder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

UNCLASSIFIED

AD 38959

DEFENSE DOCUMENTATION CENTER

FOR

SCIENTIFIC AND TECHNICAL INFORMATION

CAMERON STATION ALEXANDRIA. VIRGINIA



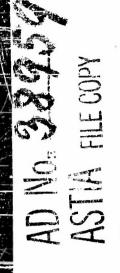
UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U.S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

THIS REPORT HAS BEEN DELIMITED AND CLEARED FOR PUBLIC RELEASE UNDER DOD DIRECTIVE 5200.20 AND NO RESTRICTIONS ARE IMPOSED UPON ITS USE AND DISCLOSURE.

DISTRIBUTION STATEMENT A

APPROVED FOR PUBLIC RELEASE;
DISTRIBUTION UNLIMITED.



Electrical Engineering Research Laboratory The University of Texas

Report No. 73

6 August 1954

Propagation of 4.3-Millimeter Radio Waves on 3.5-and 7.0-Mile Paths

Prepared Under Office of Naval Research Contract Nonr 375(01) NR 071 032

ELECTRICAL ENGINEERING RESEARCH LABORATORY THE UNIVERSITY OF TEXAS

REPORT NO. 73

6 AUGUST 1954

PROPAGATION OF 4.3-MILLIMETER RADIO WAVES ON 3.5- AND 7-MILE PATHS

by

C. W. Tolbert
C. O. Britt
C. D. Tipton
A. W. Streiton

Prepared Under Office of Neval Research Contract Nonr 375(01) NR 071 032

TABLE OF COVERNIS

		Page
	ANSTRACT	1
I.	INTRODUCTION	ì
II.	SECULIVER	2
III.	ANTINNAS	2
IV.	CALIERATED ATTENUATOR	2
Ÿ.	TRANSMI TIKR	4
άΙ°	MEASURING PROCEDURE	4
AII.	DATA	6
VIII.	SEPARATION OF WATER VAPOR AND GAYOUN LOSS	6
IX.	RADIO AND REFRACTIVE INDEX FLUCTUATIONS	10
x.	comparison with 8.6-millimeter data	14
XI.	STEMARY	14.

FIGURES

		Page
1.	View of Crystal Video Receiver	3
2.	View of Transmitter as used on 3.5-Mile Path	5
3.	View of Prenemitter as used on 7.0-Mile Fath	5
4.	3.5-Mile Path as seen from University Towns	8
5.	7.0-Mile Path as seen from University Tower	8
5.	Loss of Radio Signal For Mile vs Water Vapor Content	9
7.	Spectral Distributions of Radio Signal Strongth, Refractive Index, and Temperature	n
8.	RMS of Radio Fluctuation vs RMS of Refractive Index Fluctuation	13

ABSTRACT

Propagation measurements are reported for frequencies of 69.5 and 70.1 kilomegacycles per second over 3.5- and 7.0-mile paths in the vicinity of Austin, Texas. These measurements indicate that the cayger absorption is somewhat less than that predicted by Van Vleck [1] whereas the water vapor absorption is several times that predicted.

The magnetron transmitter, the crystal video receiver, and the associated equipment used for the tests are described in the report.

I. INTRODUCTION

The measurements described in this report using a wavelength of 4.3 millimeters are an extension of previous measurements made at 8.6 millimeters [2, 3]. The equipment for the longer wavelength had been so designed that it was readily adaptable to the 4.3-millimeter tests as described later.

A frequency of 69.5 kilomegacycles per second was used on paths 3.5 and 7.0 miles long and a frequency of 70.1 kilomegacycles per second was used on the 7.0-mile path. Data was taken using the 69.5 kmc/s signal for five minute intervals of time on ten days over the 3.5-mile path and on six days over the 7-mile path. Similar numples of data were taken on 70.5 kmc/s on ten days over the 7.0-mile path.

Humidity measurements made at both ends of the path were found to agree satisfactorily with data obtained from the Weather Bureau. By plotting the loss relative to the free space signal level as a function of the water vapor content of the atmosphere it was possible to estimate the loss due to water vapor and that due to oxygen.

The average wet and dry tulb temperature measurements made at the transmitting and receiving sites differed by less then one degree Fabrenheit from the data obtained from the Weather Bureau.

Refractometer measurements were made on a number of days and the spectral distribution of the refractive-index fluctuations is compared to the spectrum of the millimeter fluctuations.

II. RECEIVER

The receiver used to detect the 4.3-millimeter signals was of the crystal video type and is shown in Figure 1.

Through the courtesy of Nell Telephone Laboratories, one of their 5.4-millimater experimental crystale was made available for use in this receiver. This crystal was of the cartridge type and was mounted in a brass block in such a manner as to allow waveguide to be held in alignment with the windows of the crystal cartridge. One of the sections of waveguide was slotted in the plane of the electric lield and a piece of 0.005 inch thick phosphor-bronze was passed through the slot end used as an adjustable shorting stub.

An EH tuner constructed of RG-98/U silver waveguide with shorting stubs of 0.006 inch phosphor-bronze passed through slots in the E and H armes was placed between the crystal holder and the calibrated attenuator.

The antennas used were sectional cylindrical horns that had been designed to have optimum dimensions at 0.5 millimeters.

The video amplifier had a bendwidth of 15 magacycles and a minimum detectable signal level of approximately 43 dbm when used with an average video crystal, detecting a 0.25 microsecond pulse at 9.3 kms/s. The video amplifier was divided into two parts. The pre-amplifier was mounted on the base holding the trystal detector, the mi tuner, the galibrated attenuator, and the antenue. The main body of the amplifier, the integrator, the metering circuits, and the power supply were mounted on a chassis behind a relay rack panel. A 20 foot length of cable was used to couple the pre-amplifier to the main amplifier. A voltage derived from the integrator was supplied back as a bias to the stages of the main amplifier to produce a 20-db-range recording scale.

III. ANTAWAS

The antennes used on the 3.5-mile path consisted of four sections of the conical horn which gave optimum dimensions at 8.6 mm and had an antenne gain of 34 db. The antennes used on the 7-mile path consisted of eight sections of the conical horn with a hyperbolic lens of playiglass at the mouth to modify the phase front to the extent that an effective capture area of near one was realized. These antennes had a gain of \$5.0 db. The antennes used for calibrating the attenuator were single sections of the cylindrical horn so that all specings between the transmitter and receiver the phase front was essentially plane across the mouth of the antennes.

IV. CALLERATED ATTENUATOR

The calibrated attenuator was of the guillotine type with a dial gage used to indicate the depth of penetration of the resistance material. The moving parts and the blocks used to assemble the moving parts and the silver waveguide were



VIEW OF CRYSTAL VIDEO RECEIVER

FIG. 1

made of stainless steel. The glass upon which nichrome was evaporated was a 0.005 inch thick microscope slide cover. The glass was cut on an arc whose cord was 1.5 inches with a tantalum-carbide tipped scribe. The nichrome was evaporated on the glass from a tantalum boat at a chamber pressure of 5 x 10⁻⁵ millimeters of moreury after the glass had been preheated to a temperature of 200° C. The 460 ohm per square nichrome film was given a protective conting of magnesium fluoride. The glass with its coating of resistance material was camented in a slot in the guillotine with De Ebstinsky coment.

The attenuator was calibrated by varying the spacing between the transmitter and the receiver ofer such distances as to give known increments of attenuation based on the inverse square law variation of power level. This procedure was repeated a number of times over two different paths and a smooth curve was drawn through the average of the points thus obtained. The maximum deviation of the points from the average was approximately 0.5 db.

V. TRANSMITTER

The signal sources were experimental magnetrons of the Columbia University design operating at frequencies of 69.25 kmc/s and 70.10 kmc/s.

The antennas used on the transmitter were identical with those used at the receiver with the 34 db antenna on the 3.5-mile path and the 40.8 db antenna on the 7-mile path. A view of the transmitter as used on the 3.5-mile path is shown in Figure 2 and a view of the transmitter as used on the 7-mile path is shown in Figure 3. A crystal detector was used to monitor the relative peak power level and the pulse length. Power cutput characteristics relative to the average magnetron current and filement voltage were determined by measurements made over a 1000 foot path over a period of two weeks.

VI. MEASURING PROCEDURE

(a) 1000 foot Path

Measurements were made over a base path whose length was 1000 feet with the transmitter and receiver assembled as they were used on the 3.5-mile and 7-mile paths. Measurements were made at random times during a two week period. The results indicated the signal strength could be measured with an accuracy of t 0.2 db. The base path also provided a signal level relative to which the signal levels over the 3.5-mile and 7-mile path were measured.

(b) 3.5-mile and 7-mile Paths

The receiver was located on the 25th floor of the University tower for both the 3.5-mile path and the 7-mile path. This location was about 250 feet above ground level and at an elevation of about 250 feet. For the 3.5-mile path, the









VIEW OF TRANSMITTER AS USED ON 3.5-MILE PATH

<u>5</u>

transmitter was located at the antenna site of KTBC-TV on Mount Larson at an elevation of 910 feet. The ground level dropped off from the University tower, rising abruptly at Mount Larson. A view of this path as seen from the University tower is shown in Figure 4.

For the 7-mile path, the profile elevation increased fairly uniformly from the base of the tower to a value of 810 feet at the Balcones Research Center. The transmitter was located about 10 feet above ground for the measurements. The 7-mile path as seen from the University tower is shown in Figure 5. The path is the same as shown in Figure 3 of Report No. 69 [2].

Telescopic gun nights were attached to the antennas and were used for pointing the antenna each time measurements were made. After alignment, the 4.3-millimeter signal was recorded for a period of three to five minutes on an Esterline-Angus recorder.

Sling psychrometer readings at the transmitter site and at the receiver site were taken each time signal strength data were recorded. These readings were found to agree very closely with data obtained from the Weather Bureau. The difference in the water content of the atmosphere as determined from the psychrometer measurements at the two ends of the path did not exceed 0.5 gram per cubic mater. The average of the values measured at the ends of the path was assumed to be the average over the path.

Recordings were made on a number of the measurement days of the refractive-index fluctuations as given by a Grain refractometer [4]. Simultaneous recordings of temperature fluctuations were also taken using a calibrated thermister.

VII. DATA

The signal strength and water vapor data are given in Table I. The loss was measured relative to that at 1000 feet and the inverse square loss was removed to make the measurements relative to the free space value. For both paths, the signal to noise ratio was approximately 10 db. The relative measurements were made with an accuracy of ± 0.5 db.

VIII. SEPARATION OF WATER VAPOR AND OXYGEN LOSS

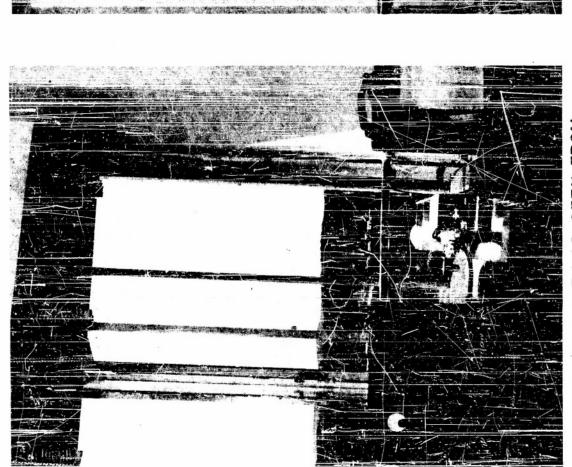
The loss in excess of the free space loss was reduced to a per mile basis and is also shown in Table I. This data was plotted as a function of the water vapor content of the atmosphere and is shown in Figure 5.

The line drawn on the figure is a least square line using all of the data on an equal basis. The root mean square of the signal deviation from this line is 0.04 db. From the y intercept, the oxygen absorption loss is indicated to be 0.0 db per mile and from the slope of the line, the water vapor absorption is indicated to be 0.04 db per mile per gram of water vapor per cubic mater. The deviation of the prints from this line are also indicated in Table I.

TABLE 1
Signal Strength Data

Frequency 70.10 Kmc/s Path Leigth 3.5 miles

Date	Time	Tem- pera- ture c _p	Water Vapor g/m ³		Strength ee Space 6b/m1le	Vertical Deviation from least mean square db/mile	Fluctuation Range Ab
11 May 1954 12 May 1954 13 May 1954 14 May 1954 17 May 1954 18 May 1954 19 May 1954 20 May 1954 21 May 1954 24 May 1954	1400 1045 1045 1460 1460 1430 1400 1450 1400	80 488 786 786 876 887 888 888 888 888 888 8	15.4 11.2 10.5 9.7 12.8 13.0 15.7 14.2 15.4	4.5 4.2 3.9 4.4 4.5 4.7 4.9 5.1	1.40 1.17 1.20 1.12 1.25 1.29 1.37 1.34 1.40	04 +.03 03 +.02 00 02 +.00 03 04 013	1.4 0.5 0.5 0.5 0.5 0.5 0.5 0.5 0.4
				ency 69.49 Longth 3.			
31 May 1954 1 June 1954 2 June 1954 3 June 1954 4 June 1954 5 June 1954	1530 1130 1430 1650 1130 1430	89 87 93 83 83 83 55	15.7 18.7 17.0 9.1 9.2 15.0	4.6 5.2 5.1 3.6 4.9	1.31 1.49 1.46 1.03 1.17	+.06 01 04 +.09 04 02	0.5 0.7 0.3 0.3 0.3 0.5
				Length 7			
7 June 1954 8 June 1954 9 June 1954 10 June 1954 11 June 1954 14 June 1954 16 June 1954 1 June 1954 1 July 1954	1730 1130 1000 0930 1130 1130 1130 0930	89.5 89.5 84.5 89.5 89.5 89.5 89.5 89.5 89.5	16.0 16.2 16.2 17.0 16.2 17.0 19.0 17.6	9.7 9.5 9.5 10.5 10.4 10.4 10.4	1.38 1.36 1.37 1.36 1.36 1.40 1.49 1.49	03 +.02 +.05 +.05 +.05 01 +.02 03 +.01	1.6 1.8 2.1 1.4 1.7 2.6 1.0 2.2 1.9

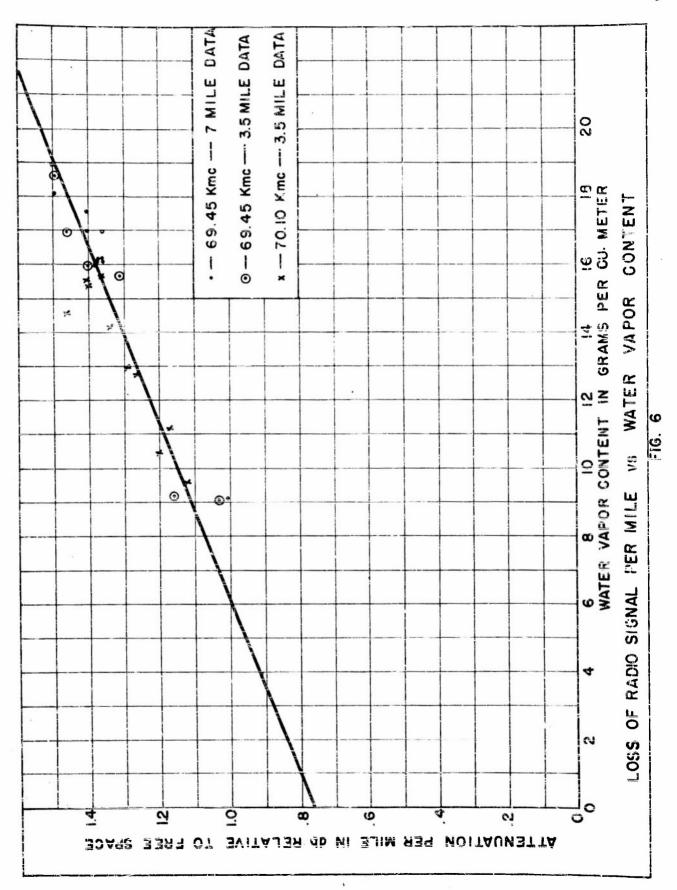


3.5-MILE PATH AS SEEN FROM

7.0-MILE PATH AS SEEN FROM UNIVERSITY TOWER

F. I.G.

UNIVERSITY TOWER



Because of the limited distribution of the points and because of the limited accuracy of the measurements, separate analysis of the data on the two frequencies did not seem desirable. A comparison of the loss obtained from Figure 5 with those predicted by Van Vleck [1] is as follows:

	<u>Maasured</u>	Predicted Theoretical Loss		
			70.10 Kmc/s	
Oxygen loss in Gb/mile Water waper loss_in	0.80 ± 0.2	1.09	0.95	
db/mile/gram/m ³	0.04 ± 0.01	0.012	0.012	

If a single line breadth constant of 0.26 is used in the formula given in reference [1], the calculated water vapor absorption would agree with the measured value of 0.04 db per mile per gram of water vapor per cubic mater.

From all of the 8.6 millimeter data previously reported, a median loss of 0.017 ab per mile per gram of water vapor per subic meter was found. The line breadth constant of 0.26 is also obtained from these data.

IX. RADIO AND REFRACTIVE INDEX FLUCTUATIONS

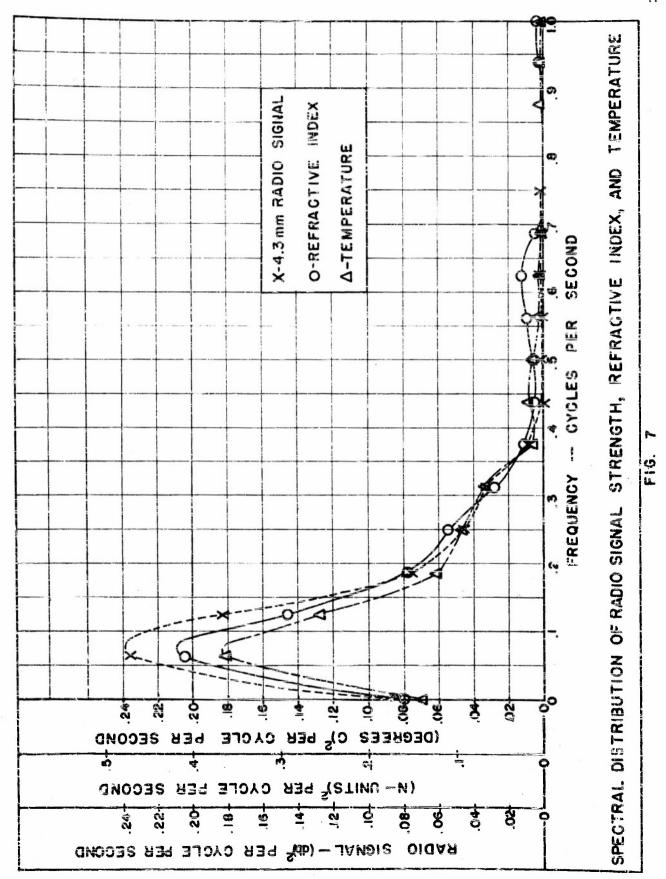
The range of signal fluctuations for each sample of data is shown in Table I. The minimum, median, and maximum fluctuation range for the two distances using the 4.3-millimeter wavelength were as follows:

Path Longth in miles	3.5	7.0
Minimum Fluotuation Range in 45	3•5 0•3	1.0
Maximum Fluctuation Range in db	1.4	2,2
Median Fluctuation Range in db	0.5	2.2 1.8

A recording microwave refractometer was set up on top of the transmitting truck and index-of-refraction data were taken simultaneously with the radio data on a number of days. Temperature fluctuations were also measured at the sampling cavity of the refractionster.

For the days on which these simultaneous data were taken, the recordings of redio signal strength, refractive index and temperature were analyzed in the following manner:

- l. The statistical distribution of the data was plotted on Gaussian paper and a straight line was drawn through the points.
- 2. The RES values of the fluctuations were obtained as one-half of the difference between the 15% and 84% points on these graphs.
- 3. Autocorrelation functions were plotted using the correlation computer developed by F. E. Brooks [5]. From these, the spectral distribution of the fluctuations were obtained. One set of these spectra is shown in Figure 7. There was



It should be noted that the length of sample was too short to determine, with any degree of accuracy, the magnitude of the very low frequency contributions. The pintercept point represents the energy in a small interval to the right of the p axis and is somewhat arbitrary in that the average value of the autocorrelation function was made zero. This difficulty does not affect the accuracy of the RMS measurement.

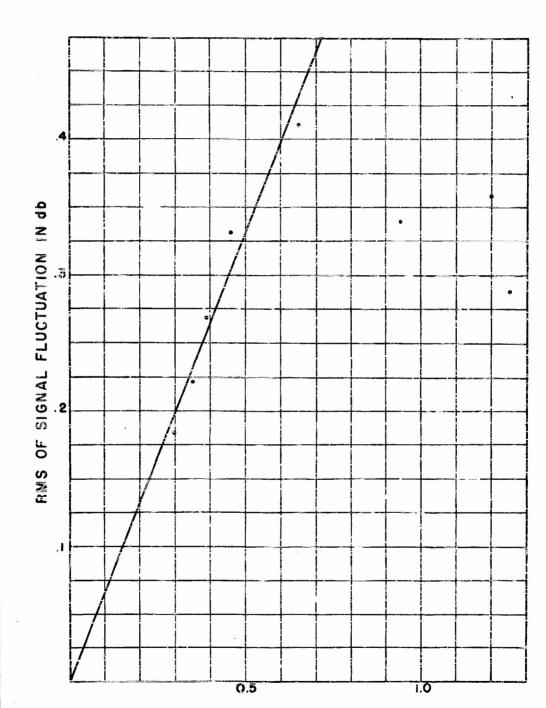
The magnitudes of the RMS values of the fluctuations for data taken on the 7-mile path were as follows:

Dete	RMS Redio	PMS Index	RMS Temperature
	Signal Fluctuations	Fluctuations	Fluctuations
	in do	in N units	in ^O C
9 June 1954 9 June 1954 10 June 1954 11 June 1954 14 June 1954 16 June 1954 18 June 1954 24 June 1954	0.22 0.33 0.18 0.29 0.41 0.27 0.34 0.36	0.35 0.46 0.30 1.48 	0.11 0.12 0.21 0.11 0.17 0.25 0.25

From these data there appear to be a definite correlation between the magnitude of the radio fluctuations and the magnitude of the index fluctuations. In Figure 8, the RMS values of the signal fluctuations are plotted as a function of RMS values of index-of-refraction fluctuations. The line shown is a least mean square drawn through the origin omitting the three points with the largest index fluctuations.

These three points do not fit the trend of the other points. In each of these three cases, however, there was a slow drift of the index on which the rapid fluctuations were superimposed. This slow drift was the predeminant factor in the RMS of the index fluctuation and had no counterpart in the radio signal fluctuations. It is therefore felt that the slow change in index of refraction had little effect on the radio fluctuations, but that the rapid index changes were very closely related to the radio fluctuations.

Another type of signal strength fluctuation was noted over the 1000 foot calibration path when antennas with beam widths of the order of 10 degrees were used. This signal strength fluctuation of 2 db was associated with the wind blowing the 18 inch high grass on the path and was of a much higher frequency than that observed over the longer paths. The signal strength fluctuations over the 1000 foot path were reduced to 0.3 db with the grass uncut by using the 1.7 degree antennas used for measurements over the 7-mile path. The fluctuations were reduced to 0.3 db with the 100 entenna by cutting the grass.



RMS OF INDEX FLUCTUATIONS IN N UNITS

RMS OF RADIO FLUCTUATIONS vs. RMS OF REFRACTIVE INDEX
FLUCTUATIONS

K. COMPARISON WITH 8.6-MILLIMETER DATA

Data were taken in March and April 1955 over the same two paths at a frequency of 35 kmc/s. At this frequency, the absorption loss was much less than for the 4.3 millimeter measurements. The median fluctuation range was, however, approximately the same for the 8.6 millimeter than for the 4.3 millimeters.

A taiwler comparison of these data are as follows:

Path Longth in miles	3.5	3.5	7.0	7.9
Wave Langth in millimeters	4.3	8.6	4.3	6.6
Number of Samples	16	6	10	19
Median Signal Level in db				
below free space	4.5	ნ•მ	9•7	1.7
Median Fluctuation range	0.5	0.8	1.8	1.0

XI. SUMMARY

Propagation measurements made at frequencies of 69.45 and 70.10 kilomegacycles per second indicated that the absorption loss was approximately that predicted by theory. It was indicated, however, that the measured absorption due to oxygen was somewhat less than the theoretical and that the measured water vapor absorption was several times higher than that predicted by present theory.

Signal level fluctuations are interpreted as being due to index-of-refraction fluctuations.

REFERENCES

- 1. Kerr, D. E., Editor, "Propagation of Short Radio Waves," Chapter S. Massachusetts Institute of Technology, Radiation Laboratory Saries, No. 13, McGraw-Hill Co., 1951.
- 2. Tolbert, C. W., Straiton, A. W., Tipton, C. D., "Propagation Studies at 8.6-Millimeter Wavelength on 3.5-, 7- and 12-Mile Paths," Report No. 69, Klectrical Engineering Research Laboratory, The University of Texas, 6 May 1953.
- 3. Tolbert, C. W., Straiton, A. W., Tipton, C. D., "Propagation of 8.6-Millimeter Radio Waves Over a 50 Mile Path," Report No. 70, Electrical Engineering Research Laboratory, The University of Texas, 26 June 1953.
- 4. Crain, C. M., Gerhardt, J. R., "The Direct Measurement of the Variations in the Index-of-Refraction of Atmospheric Air at Microwave Frequencies," Report No. 30, Klectrical Engineering Research Laboratory, The University of Taxos, 15 April 1950.
- 5. Brooks, F. E., Jr., Smith, H. W., "A Computer for Correlation Functions,"
 Report No. 50, Electrical Engineering Research Laboratory, The University
 of Texas, 1 May 1950.

DISTRIBUTION LIST

Nonr	375	(01)

Addressee	Attention, Code	No. of Copies
	Avverture out	no. of other
DEPARTMENT OF THE ARMY		
Engineering & Technical Division Office of the Chief Signal Officer Department of the Army Washington 25, D. C.	SIGOL-2 SIGET	1
Director of Research Signal Corps Engineering Laboratories Fort Monmouth, New Jersey		1
DEFARTMENT OF THE NAVY		
Chief of Naval Research Department of the Navy Washington 25, D. C.	Code 427 460 416	2 1 1
Director Naval Pasearch Laboratory Washington 25, D. C.	Code 2000 185-A 3460	6 3 1
Chief, Bureau of Ships Department of the Navy Washington 25, D. C.	Code 810 830-C	1
Chief, Bureau of Aeronautics Department of the Navy Washington 25, D. C.	EL 90 EL 90	
Chief, Bureau of Ordnance Department of the Navy Washington 3, D. C.	Re 4f	1
Chief of Naval Operations Department of the Navy Washington 25, D. C.	Op 2092 Op 55F Op 413	1 1. 1
Director Office of Naval Research Branch Office 346 Broadway New York 13, New York		1
Director Office of Navel Research Branch Office The John Grerar Library Bldg. 86 East Randolph Street Chicago, Illinois		2

DEPARTMENT OF THE NAVY (Cont'd)

Director Office of Naval Research Branck Office 1030 E. Green Street Pasadena 1, California		1
Director Office of Naval Research Branch Office 1000 Geary Street San Francisco 9, California		1
Officer-in-Charge Office of Naval Research Navy #100 Fleet Post Office New York, New York		1
Commanding Officer U. S. Naval Understar Sound Laboratory New London, Connecticut		l
Commanding Officer Naval Air Development Center Johnsville, Pennsylvania	AAFL	1
Director Naval Ordnance Laboratory White Oak, Maryland		1
Commanding Officer U. S. Naval Ordnance Test Station Inyckern China Lake, California		1
Commanding Officer U. S. Naval Postgraduets School Monterey, California	Librarian	Ī
Director Naval Electronics Laboratory San Diego 52, California	Dr. J. B. Smyth	1
DEPARTMENT OF THE AIR FONCE		
Commanding General 3151st Electronics Group Griffies Air Force Base Rome, New York	EADER	ì
Commanding Officer Air Porce Cambridge Research Center 230 Albany Street Cambridge, Massachusetts		2

DEPARTMENT OF THE AIR FORCE (Contid) Commanding General AU-AS/4: AFDRE 1 Headquarters, USAF Washington 25, D. C. Commanding General Electronics 1 Wright Air Development Center Subdivision Wright-Patterson Air Force Base Dayton, Ohio Communication Paul W. Springer 2 Wright Air Development Center WCLRD Wright-Patterson Air Force Base, Ohio DEPARTMENT OF COMMERCE U. S. Weather Bureau Director, Radar 1 Department of Commerce Engineering Washington, D. C. Boulder Laboratories Radio Division 1 National Bureau of Standards P. O. Box 299 Boulder, Colorado Office of Technical Services I Department of Commerce Washington 25, D. C. Director 1 Central Radio Propagation Laboratory National Bureau of Standards Washington 25, D. C. MISCRILANEOUS Dr. J. E. Boyd 1 Georgia School of Technology Atlanta, Georgia Department of Electrical Engineering Dr. S. S. Atwood 1 University of Michigan Ann Arbor, Michigan Research Laboratory of Electronics H. Zimmerman ì Massachusetts Institute of Technology Cambridge, Massachusetts Federal Communications Commission Technical Infor-7

mation Division

Pennsylvania Ave. & 12th St., N.W.

Washington 25, D. C.

MISCELLANEOUS (Cont'd)

Department of Electrical Engineering University of California Berkeley 4, California	T. C. McFarland	1
Propagation Laboratory School of Engineering Stanford University Palo Alto, California	Dean F. E. Terman	1
British Commonwealth Scientific Office 1800 K Street, N. W. Washington, D. C.		2
Director Froject Hermes General Electric Research Laboratory The Knolls Schenectady, New York		1
Bell Telephone Laboratories Red Bank, New Jersey	R. T. Friis	1
RCA Laboratories Division Eadio Corporation of America Princeton, New Jersey	Dr. H. H. Beverage	1
Electrical Engineering Research Laborat University of Illinois Urbana, Illinois	ory E. C. Jordan	1
Armed Services Technical Information Ag Document Service Center Knott Building Dayton 2, Ohio	rency	5
Cruft Laboratory Room 303A, Pierce Hall Harvard University Cambridge 38, Massachusetts	Mrs. M. L. Cox, Librarian	1
School of Electrical Engineering Cornell University Ithaca, New York	Prof. C. E. Burrows	1
Commandant U. S. Coast Guard Washington 25, D. C.	EEC	1
Project Lincoln, M.I.T. P. O. Box 390 Cambridge 39, Massachusetts	T. J. Carroll	

MISCELLANEOUS (Cont'd)

Department of Electrical Engineering California Institute of Technology Pasadena, California	Dr. C. H. Papas	1
Applied Physics Laboratory Johns Hopkins University 8621 Georgia Avenue Silver Spring, Maryland	George Seielstad	1
Dr. Morris Kline Institute of Mathematical Sciences Division of Electromagnetic Research New York University 23 Waverly Place New York 3. New York		1.